



SNC • LAVALIN

Impact of High Short-Circuit Current on Air Insulated Station Strain Bus Design

2016 CIGRE-IEC Colloquium

Montreal, QC, Canada

JAY TAILOR & BHARAT BHATT

Hydro and Power Delivery

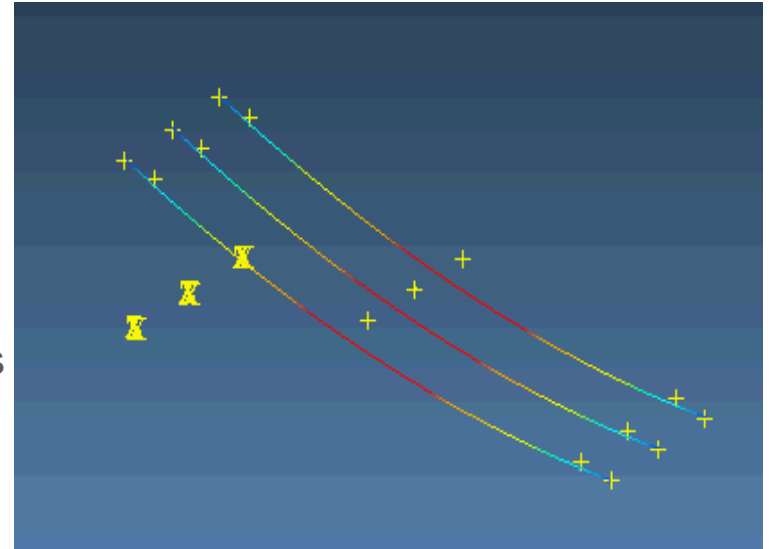
SNC LAVALIN Inc.,

Canada

Characteristics of SC Forces on Strain Bus Systems

Nature

- › Oscillatory & non-linear:
 - › Instantaneous SC Current value
 - › Ever-changing phase-phase clearance
 - › Elastic and Thermal expansion of conductors
 - › Tensile Forces in the conductors
 - › Poor rigidity compared to Rigid Bus



Effects

- › Tensile Forces in the conductors, terminations and associated hardware
- › Elastic or Plastic deformation of conductors
- › Structure deflection
- › Conductor oscillations – Can compromise minimum clearances



Types of SC Forces on Strain Bus Systems

Pinch Effect Force

- › Tensile Force due to attraction between bundled conductors

Shor-Circuit Force

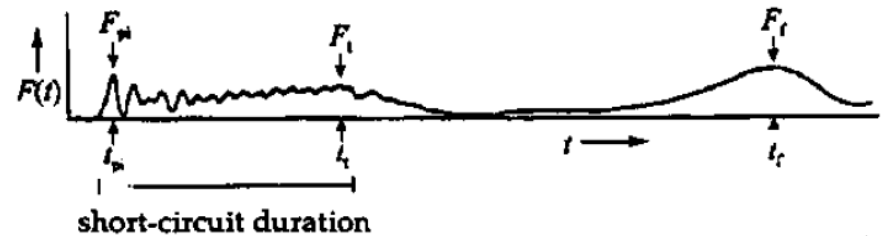
- › Tensile Force due to attraction or repulsion between Phase conductors

Dropback Force

- › Tensile Force when conductor drops back after clearance of short circuit

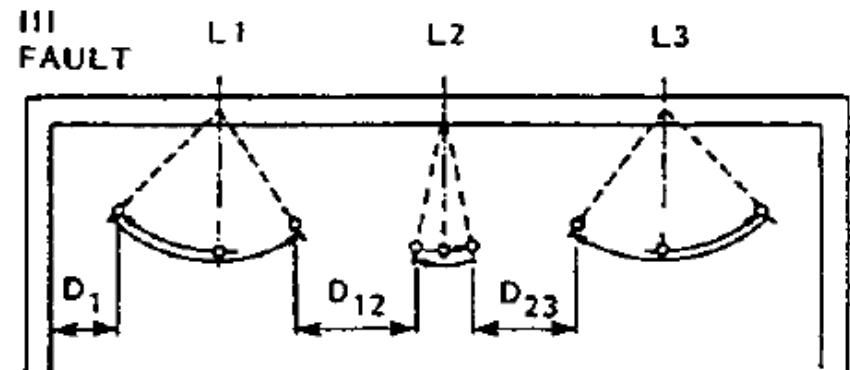
Horizontal Displacement

- › Maximum displacement (swing) of phase conductors from the resting position



F_{pi} Pinch force
 F_t Short-circuit
 F_f Drop force

Source : CIGRE Brochure 105

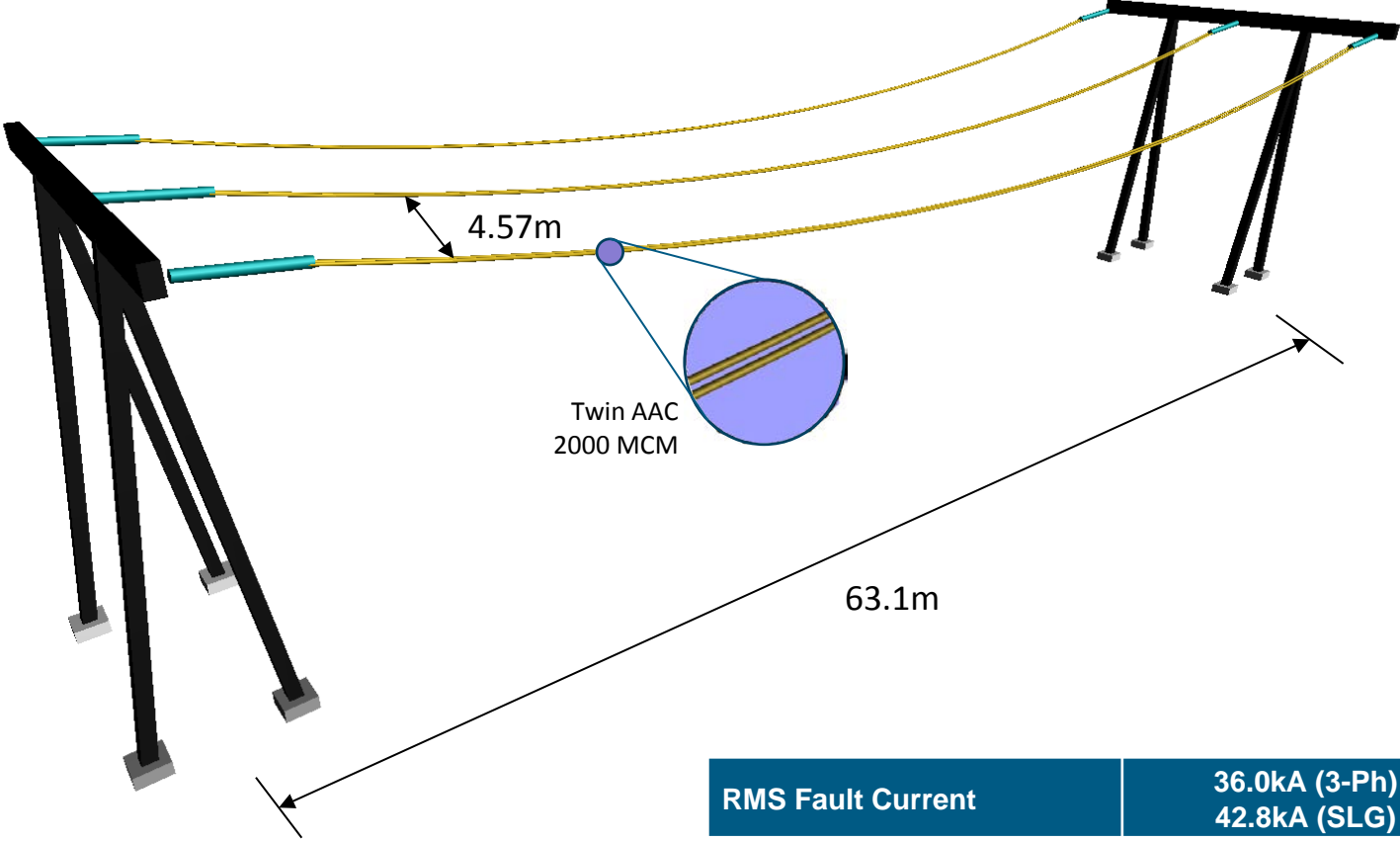


Source : CIGRE Brochure 105

Available Tools for Analysis

1. Simplified Hand Calculations – IEC 60865-1
2. Simplified Hand Calculations – IEEE 605-2008
3. Finite Element Analysis

230kV Strain Bus Study Case Details



| | |
|-------------------------------|---------------------------------------|
| RMS Fault Current | 36.0kA (3-Ph) 42.8kA (SLG) |
| Fault current duration | 0.484 seconds |
| System Frequency | 60 Hz |
| X/R ratio | 42.1 |

Results

| Short Circuit Forces | Temperature | IEEE 605 (N) | FEA (N) | IEC 60865 (N) |
|--|-------------|--------------|---------------|---------------|
| Maximum tensile short circuit force during fault current, F_t (N) | -20°C | 30,846.2 | 29,000 | 30,193.4 |
| | -50°C | 38,807.4 | 40,100 | 37,612.9 |
| | 90°C | 18,753.7 | 18,125 | 18,612.9 |
| Maximum tensile short circuit force when conductors drop back, F_f (N) | -20°C | 130,135.1 | 55,500 | 90,037.1 |
| | -50°C | 121,057.6 | 74,375 | 88,588.1 |
| | 90°C | 149,505.1 | 26,250 | 95,335.1 |
| Maximum tensile force caused by Pinch effect F_{pi} (N) | -20°C | 101,884.9 | Indeterminate | 65,836.6 |
| | -50°C | 107,339.3 | Indeterminate | 74,185.1 |
| | 90°C | 94,723.8 | Indeterminate | 54,621.0 |

| Diplacements | Temperature | IEEE 605 (m) | FEA (m) | IEC 60865 (m) |
|--|-------------|--------------|---------|---------------|
| Maximum horizontal displacement within a span, b_h (m) | -20°C | 1.01 | 1.3 | 1.04 |
| | -50°C | 0.815 | 1.13 | 0.866 |
| | 90°C | 1.542 | 2.0 | 1.556 |
| Minimum phase to phase clearance during fault condition, a_{min} (m) | -20°C | 2.552 | 3.1 | 2.482 |
| | -50°C | 2.939 | 3.5 | 2.838 |
| | 90°C | 1.487 | 2.3 | 1.459 |



Results (Contd.)

| Required Ratings | Per IEEE 605 | Per IEC 60865 | Per FEA |
|--|----------------|----------------|--------------|
| ANSI/IEC Strength Class of Strain Insulator | CS-13 (150 KN) | CS-11 (111 KN) | CS-8 (80 KN) |
| Maximum Design Force to be considered for Support Structure design | 450 KN | 202 KN | 160 KN |

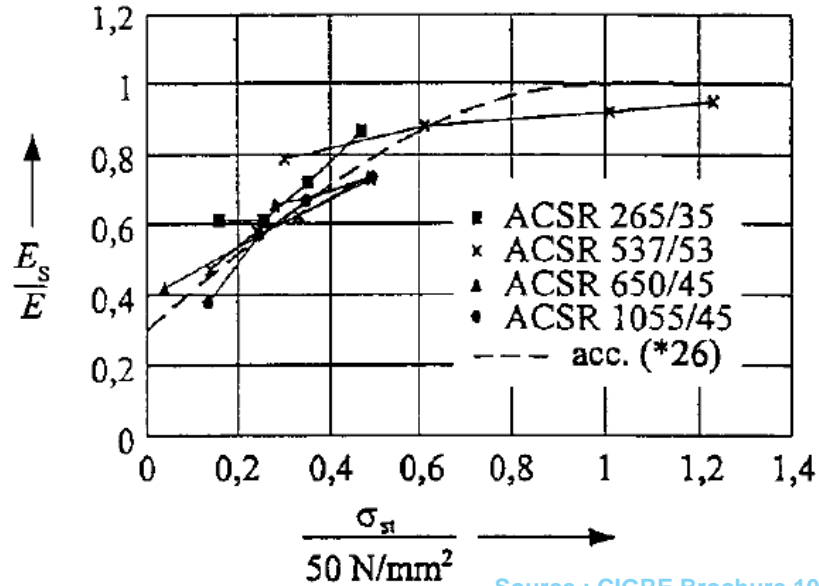
Which one to follow?

Observations

- › Short Circuit Forces (F_t) matches well among all three methods
- › Phase clearances are found to be larger in FEA; IEC and IEEE results are consistent
- › Significant difference in Dropback forces
- › Although not so close, FEA results are closer to IEC than IEEE
- › Designing systems according to IEEE forces maybe challenging and uneconomical
- › IEEE method derived from IEC 60865 – Apparently not so!

Differences between IEEE and IEC methods

1. Conductor Flexibility: IEEE assumes a Constant Young's Modulus unlike IEC according to which Young's modulus is non-linear.



This means the conductor are more elastic for lower stresses thus can absorb relatively more forces.

Source : CIGRE Brochure 105

Differences between IEEE and IEC methods (contd.)

2. Support Structure Flexibility:

IEC considers Supports to be Flexible; IEEE considers Supports to be Rigid

$$N = \frac{1}{S l} + \frac{1}{n E_{\text{eff}} A_s} \quad \text{IEC}$$

← Support Structure Stiffness

$$N = \frac{1}{k_{eq} l}$$
$$\frac{1}{k_{eq}} = \frac{1}{k_c} + \frac{2}{k_i} \quad \text{IEEE}$$

This means the Support structure absorbs some of the forces in IEC methodology. Not so in IEEE methodology.



Differences between IEEE and IEC methods (contd.)

3. Selection of design Forces for Support Structures:

IEC Methodology: Twice the largest of (F_t, F_f, F_{pi}) + One times Static tensile force

IEEE Methodology: Thrice the largest of (F_t, F_f, F_{pi})

*Much stronger Support structure
required in IEEE methodology*



Closing Remarks

- The paper presents a comparison of IEEE, IEC and FEA methods for Short circuit forces
- Fundamental differences were found between how two methods treat some parameters
- Difference between IEEE and IEC results are large – IEEE results are generally of larger magnitude
- It is recommended that IEEE 605 methodology be harmonized with IEC 60865

Questions??

